

Groundwater extraction with minimum cost.

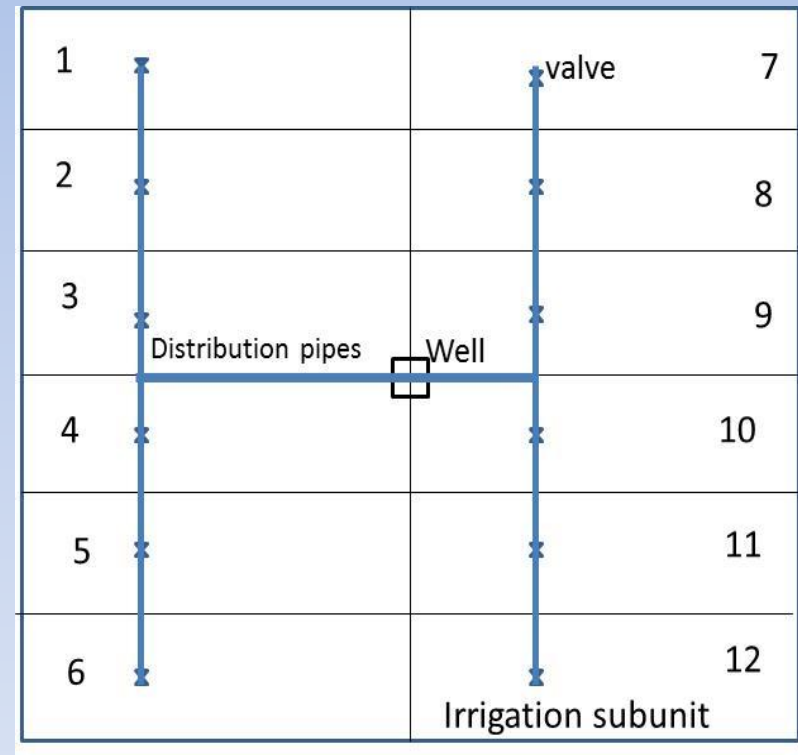
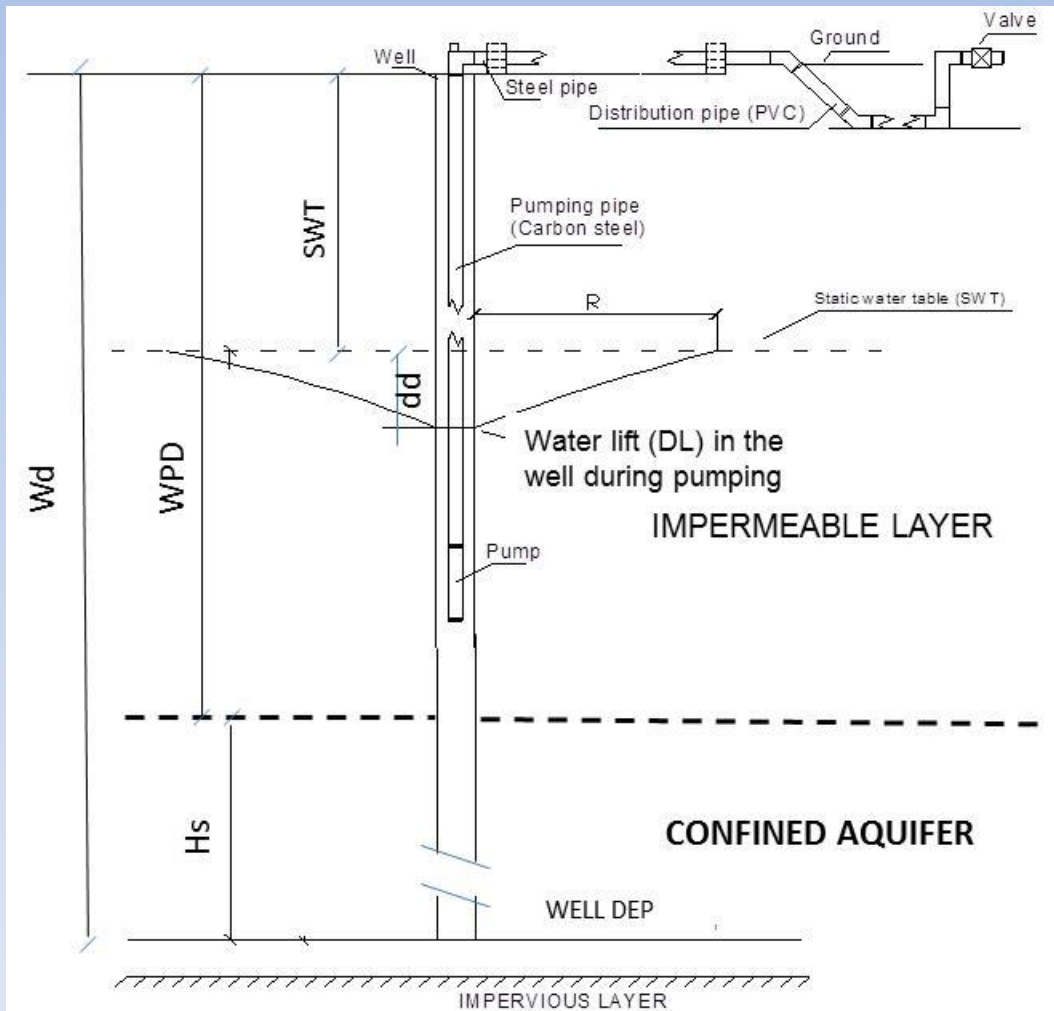
OBJETIVO

- Minimize the total cost (C_T) of **water abstraction and application** with the irrigation system (investment (C_a) + operation (C_{op}) developing a tool for decision support named **DC-WAT** (Design of pressurized irrigation), analyzing the irrigation system as a whole, from the water source to the emitter, **integrating the main factors** implied in the process.
- **Apply DC-WAT** to sprinkler and drip irrigations using groundwater from two types of aquifer for corn, piper and vineyard crops in Spain.

METHODOLOGY



Diagram of the infrastructure to design



METODOLOGIA

Main novelties and innovations introduced by DC-WAT :

- To consider the **water abstraction and its application as a whole**.
- Determines the **type of pump** and estimate fluctuations in the SWT during the irrigation season.
- To select the **design** and management of **irrigation subunit** leading to a minimum C_T
- Have into account the type of aquifer and obtain the **optimum drilling and pumping pipe diameters**.
- Select the power access and the moment to work during the irrigation season to **minimize the energy** and investment costs.

METHODOLOGY: Optimization process in **DC-WAT**

Investment cost of
irrigation subunit



PRESUD

Model for optimum designing of
irrigation systems at plot level

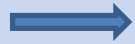


Characteristic and
efficiency curves of
pump



Model for optimum sizing of
water distribution network to the
irrigation subunit

Aquifer data



Optimization
variables

- **C**
- Pumping pipe
- Water distribution network



Working
conditions for
each month in
irrigation season



Investment cost



**MINIMUM
TOTAL COST**



Crop data

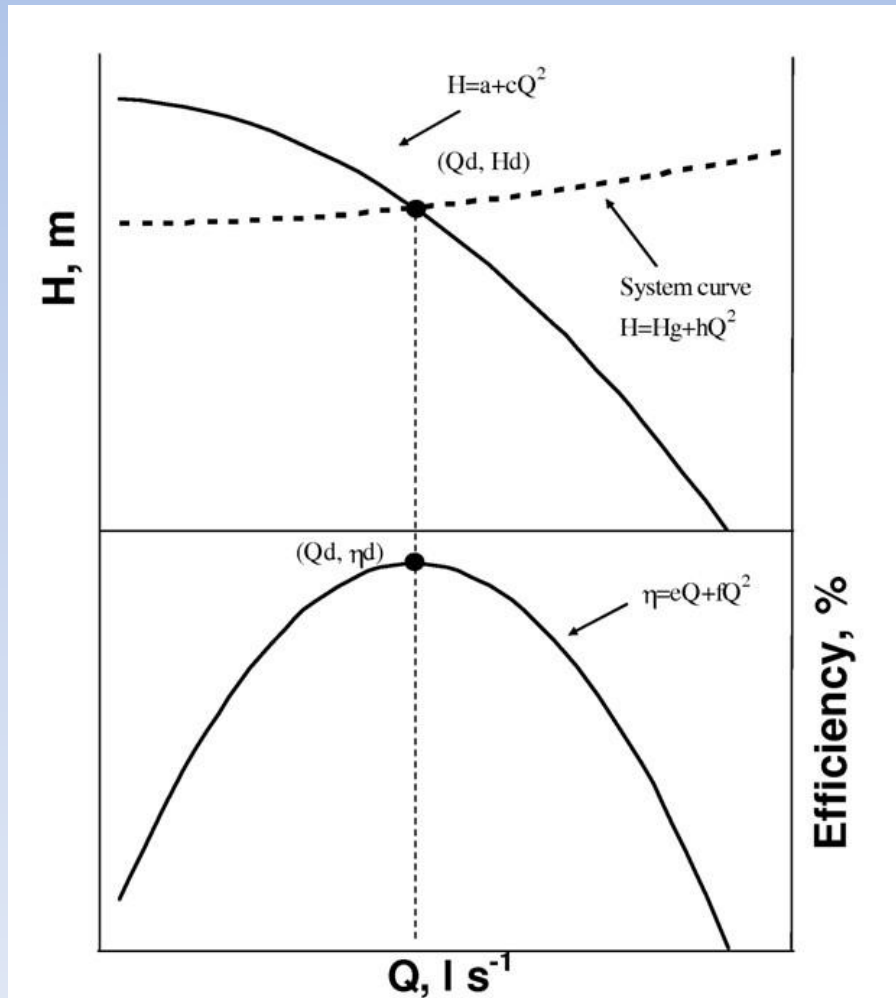


Energy cost



Metodología

Curvas características Q-H y Q- η de las bombas



$$H = a + cQ^2$$
$$\eta = eQ + fQ^2$$

METODOLOGIA

Optimization process (Downhill Simplex method)

Objective
function

$$\text{MIN } (C_a + C_{op})$$

$$C_{inv} = C_{pump} + C_{pi} + C_{pp}$$

$$C_{pump} = g N_B^3 + h N_B^2 + k N_B$$

$$C_{pi} = l D_{dist}^m$$

$$C_a = C_{inv} CRF$$

$$C_{op} = \sum_{i=1}^{12} \sum_{j=1}^k (N_p)_i Pa_{ij} + \sum_{i=1}^{12} \sum_{j=1}^k (N_p)_i T_{ij} P_{ij}$$

$$N_B = \frac{9,81 Q H}{\eta}$$

T = monthly operation time
P = energy price (€/kWh)

Optimization variables : c coefficient , D_{dist} and D_{dist}

Values of the different parameters related with the sprinkler irrigation system

Spacing of sprinklers (m x m)	h_a (kPa)	E_a (dimensionless)	AR_a (mm h ⁻¹)	Diameter of Nozzles (mm)	Corn gross water requirement m ³ ha ⁻¹ yr ⁻¹
18 x 18	300	0.77	5.90	4,8+2.4	8,249
	350	0.79	6.33	4,8+2.4	8,049
15 x 15	350	0.82	8.00	4,4+2.4	7,766

Corn net water requirement 6500 m³ha⁻¹yr⁻¹

Values of the different parameters related with the drip irrigation system pepper and vineyard crops

Parámetro	Valores en las condiciones de referencia	
	pepper	vineyard
Pendiente del terreno	0%	
X	0.5	
CV _{qmf}	0.05	
D _{ramal} (nominal) PE 0.25MPa	16 mm	
Nivel dinámico (ND)	60 m	
Superficie de la parcela (S)	10 ha	
Longitud de línea eléctrica de MT	1 km	
Separación entre plantas	0.4 m	1.5 m
Necesidades netas de riego anuales (R _n)	5900 ⁽¹⁾ m ³ ha ⁻¹ Y ⁻¹	1500 ⁽¹⁾ m ³ ha ⁻¹ Y ⁻¹
Caudal del emisor (q _a)	2 L h ⁻¹	4 L h ⁻¹
Separación entre emisores	0.75 m	1.25 m
Separación entre laterales	1.0 m	3.0 m
Relación de transpiración (Tr)	1.05	1.0

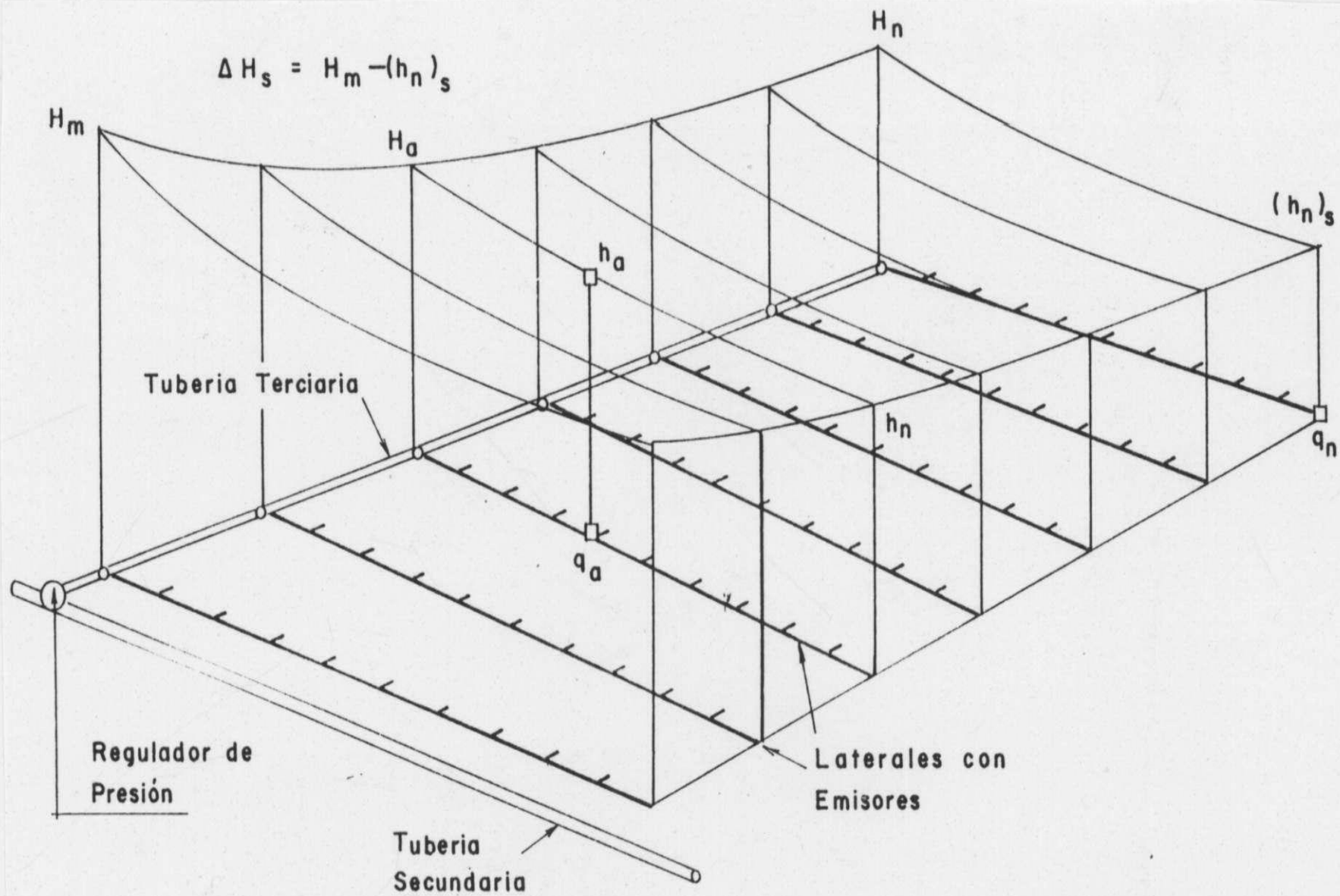
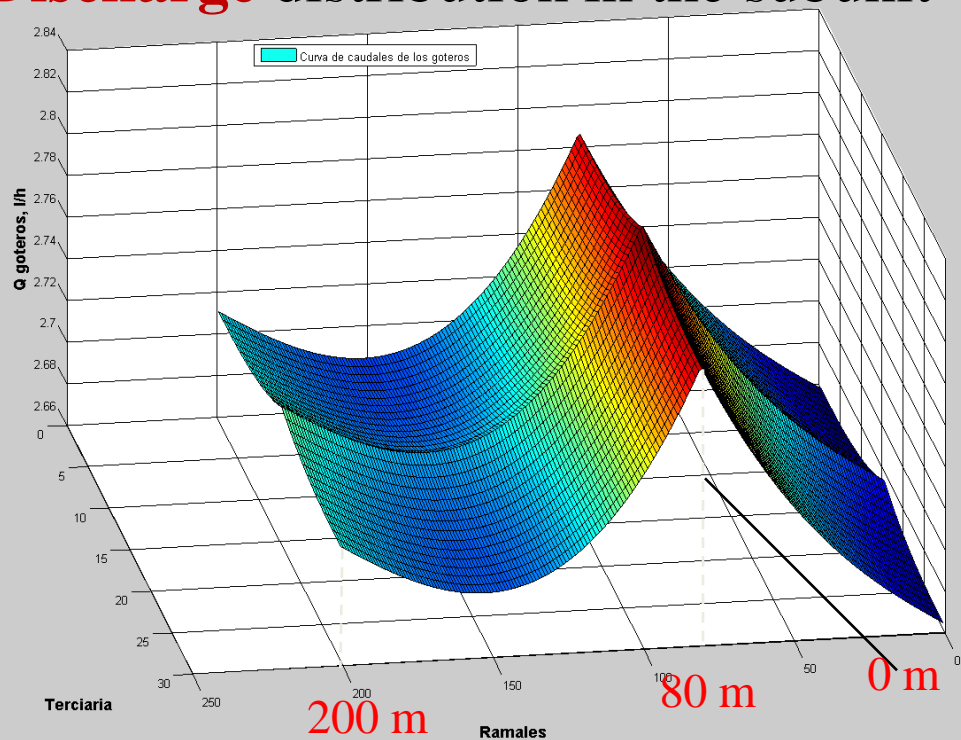


Fig. 17.2 Distribución de presiones en una subunidad de riego en terreno horizontal.

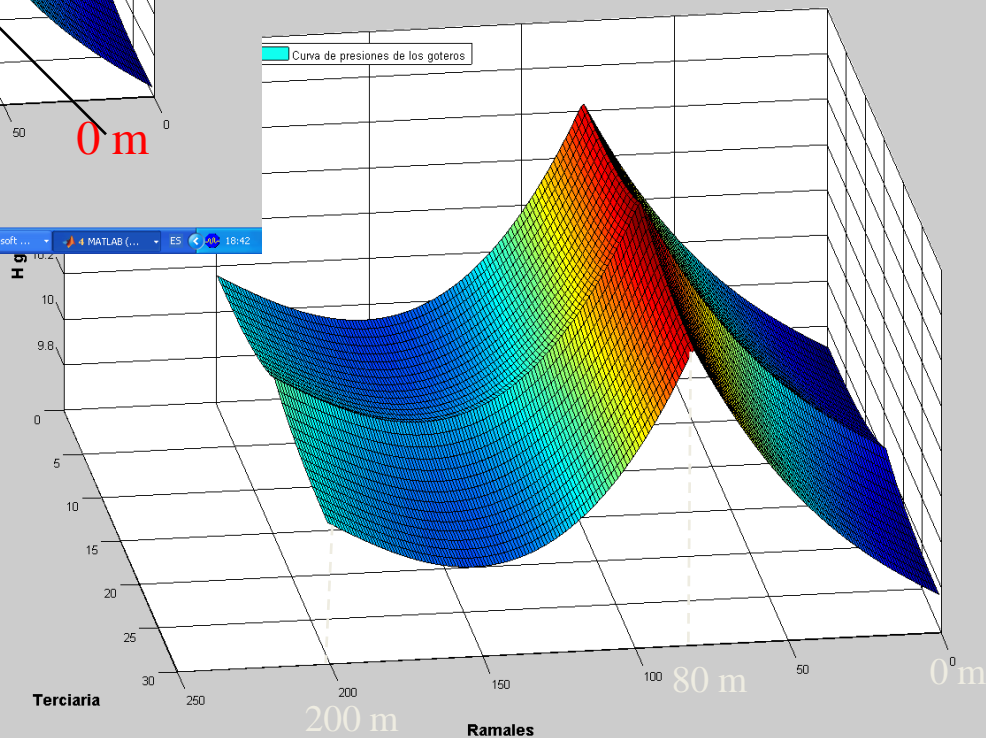
Figure 1

Discharge distribution in the subunit

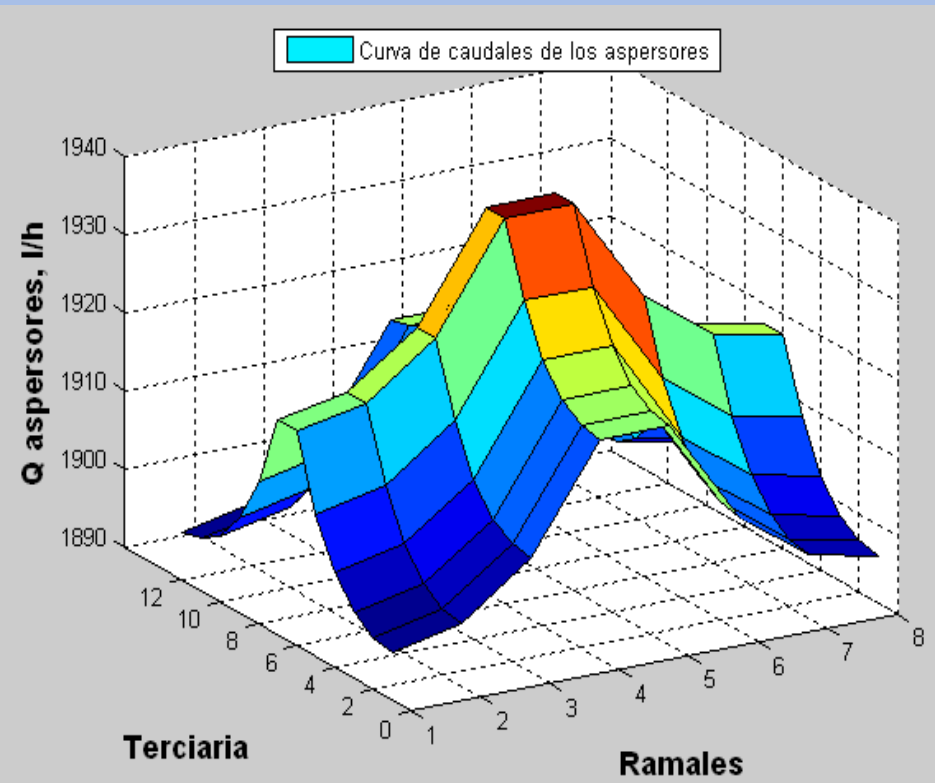


Lateral slope: 1%
Manifold slope: 0%

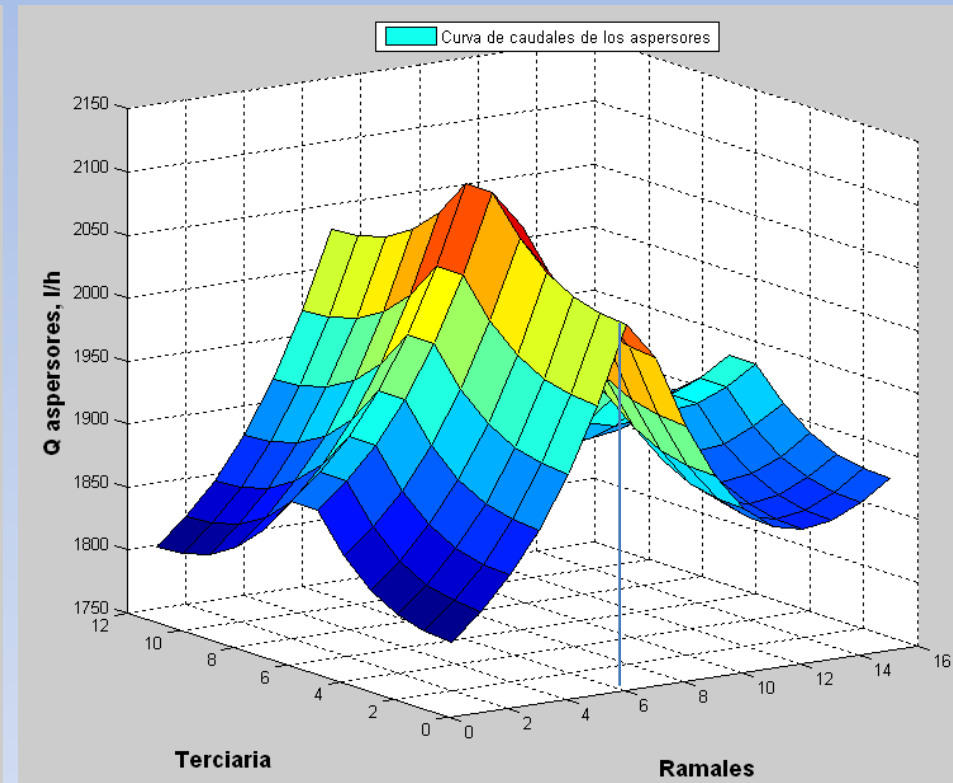
Pressure head distribution



Discharge distribution of the sprinkler for 18x18 spacing and $H_o = 350$ kPa



EU= 97.3% and $\Delta q=2.3\%$



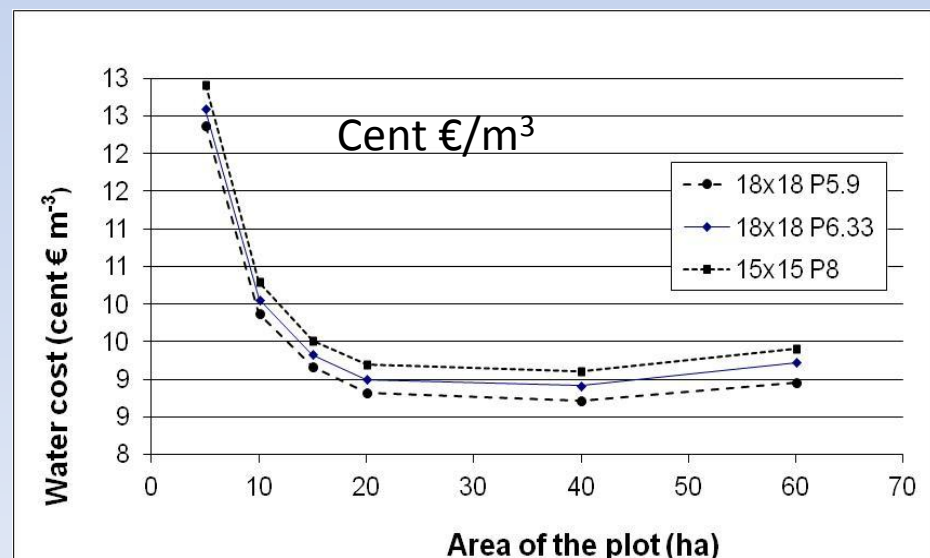
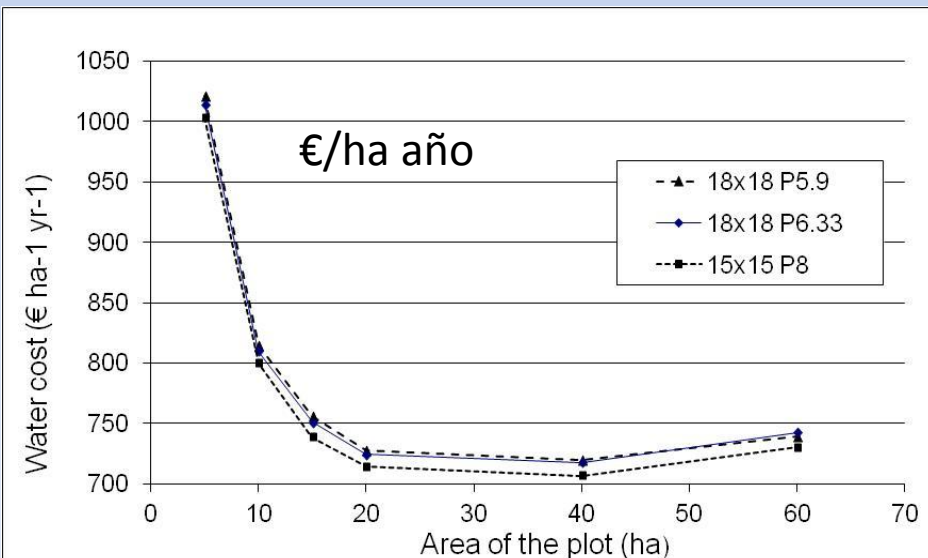
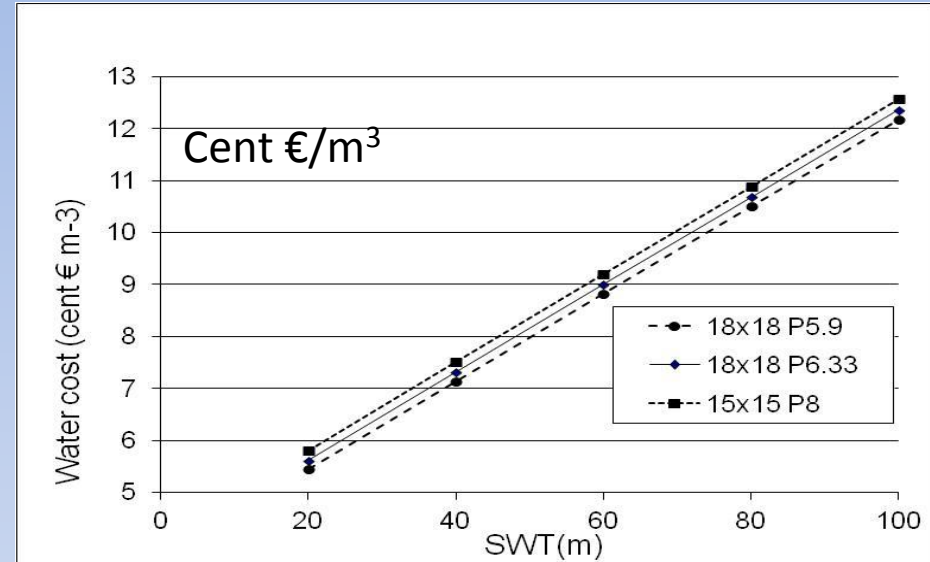
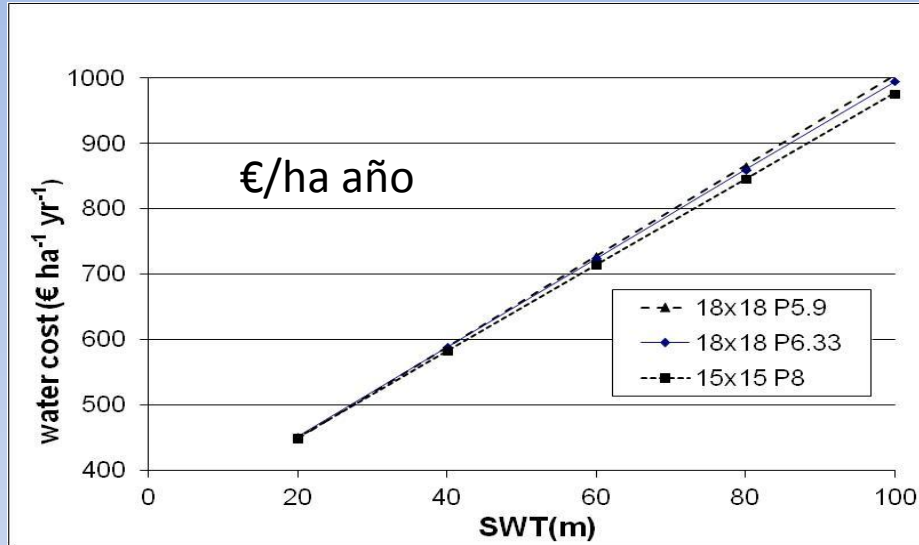
EU= 92.3% and $\Delta q=15.7\%$

- (a) 3.1 ha (12 laterals with 8 sprinkler each) and $S_{o1}=0\%$,
(b) 6.2 ha (12 laterals with 16 sprinklers each) and $S_{o1}=3\%$, 0 m
200 m

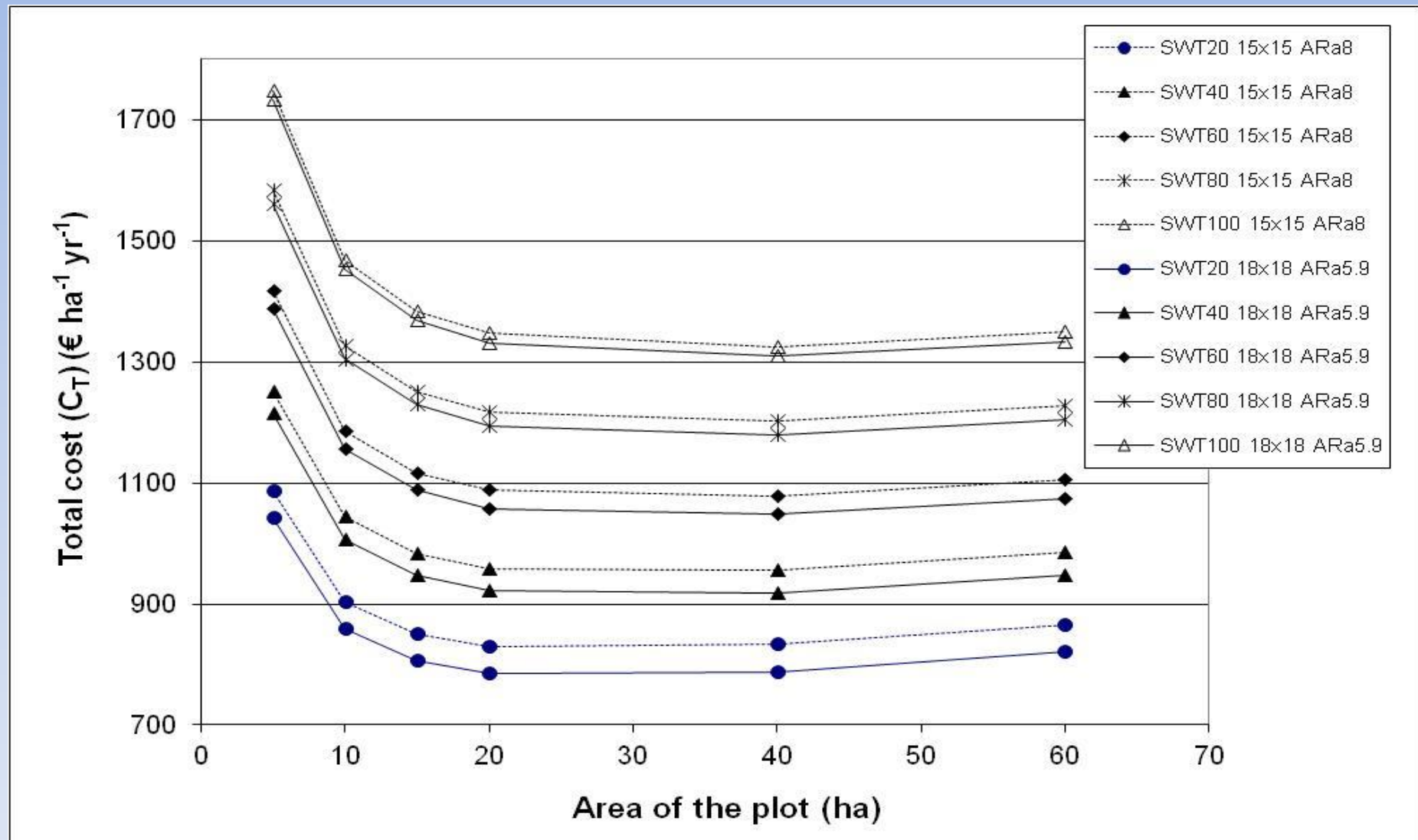
RESULTS



Cost of water transport from the source to the subunit inlet (C_w), for a corn crop in the unconfined aquifer

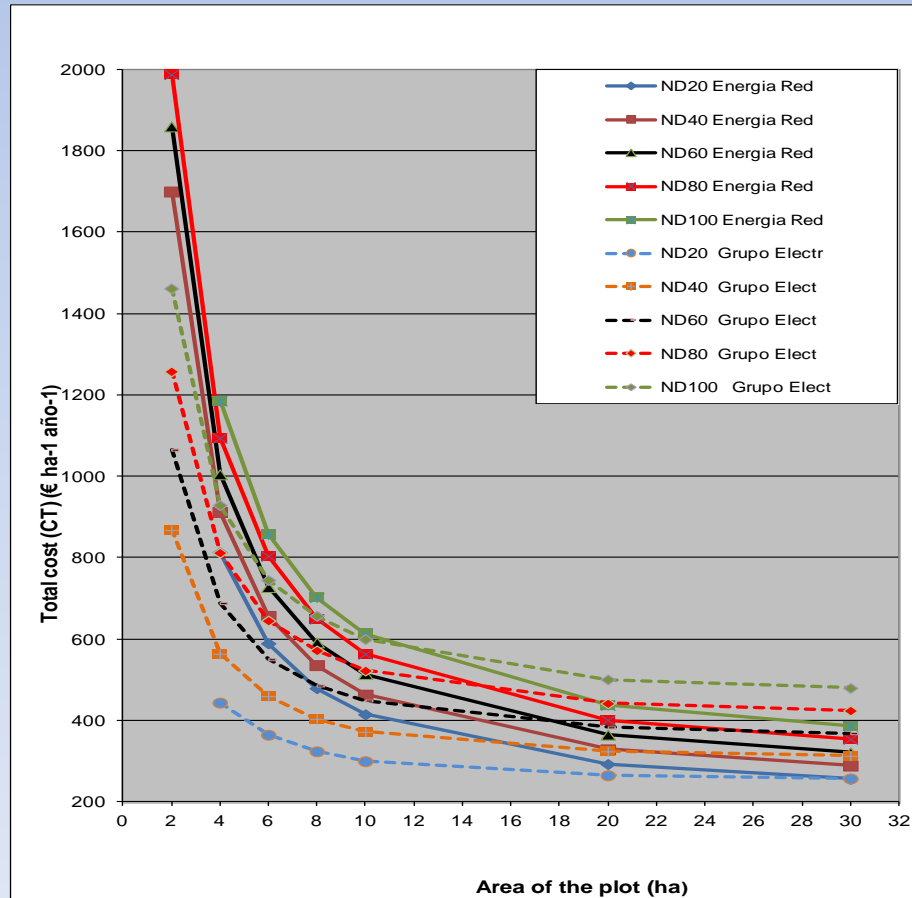
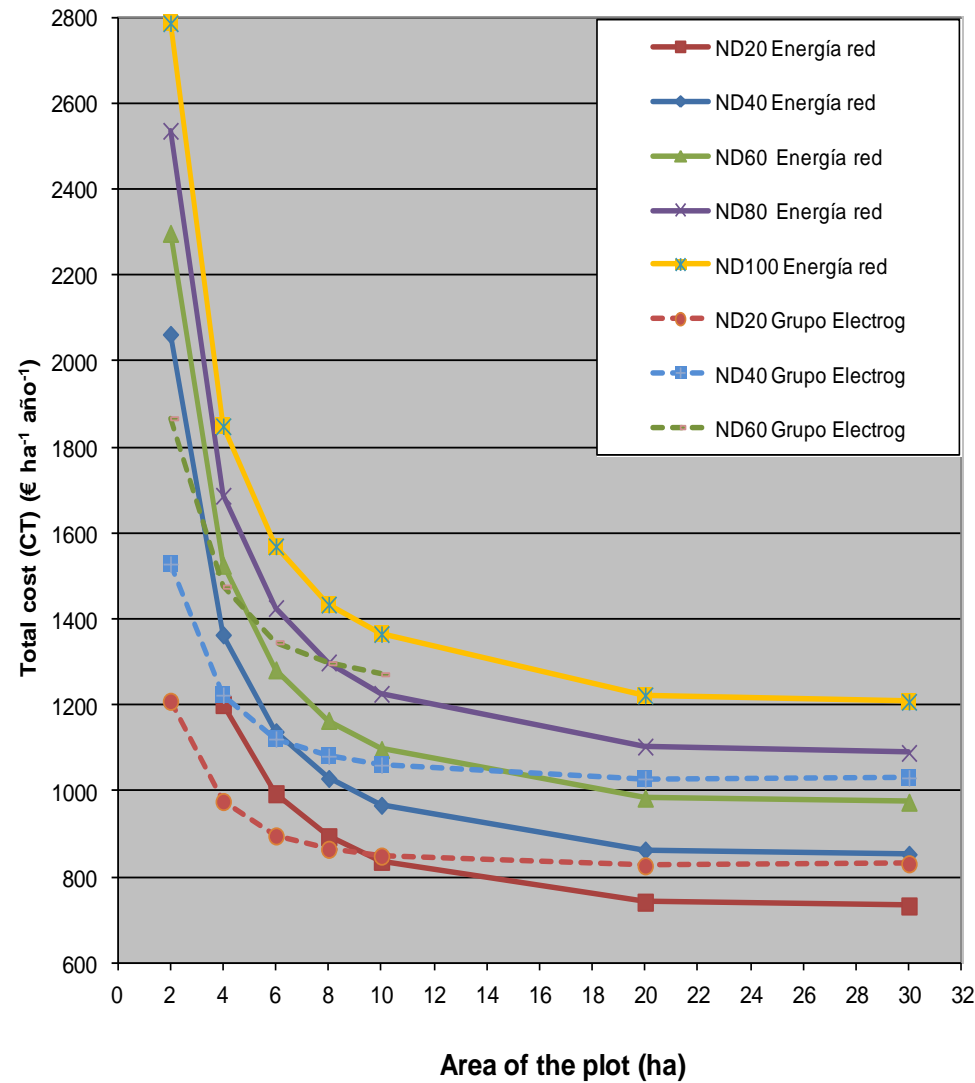


Pattern of C_T with the S for different sprinkler spacing and SWT in the unconfined aquifer

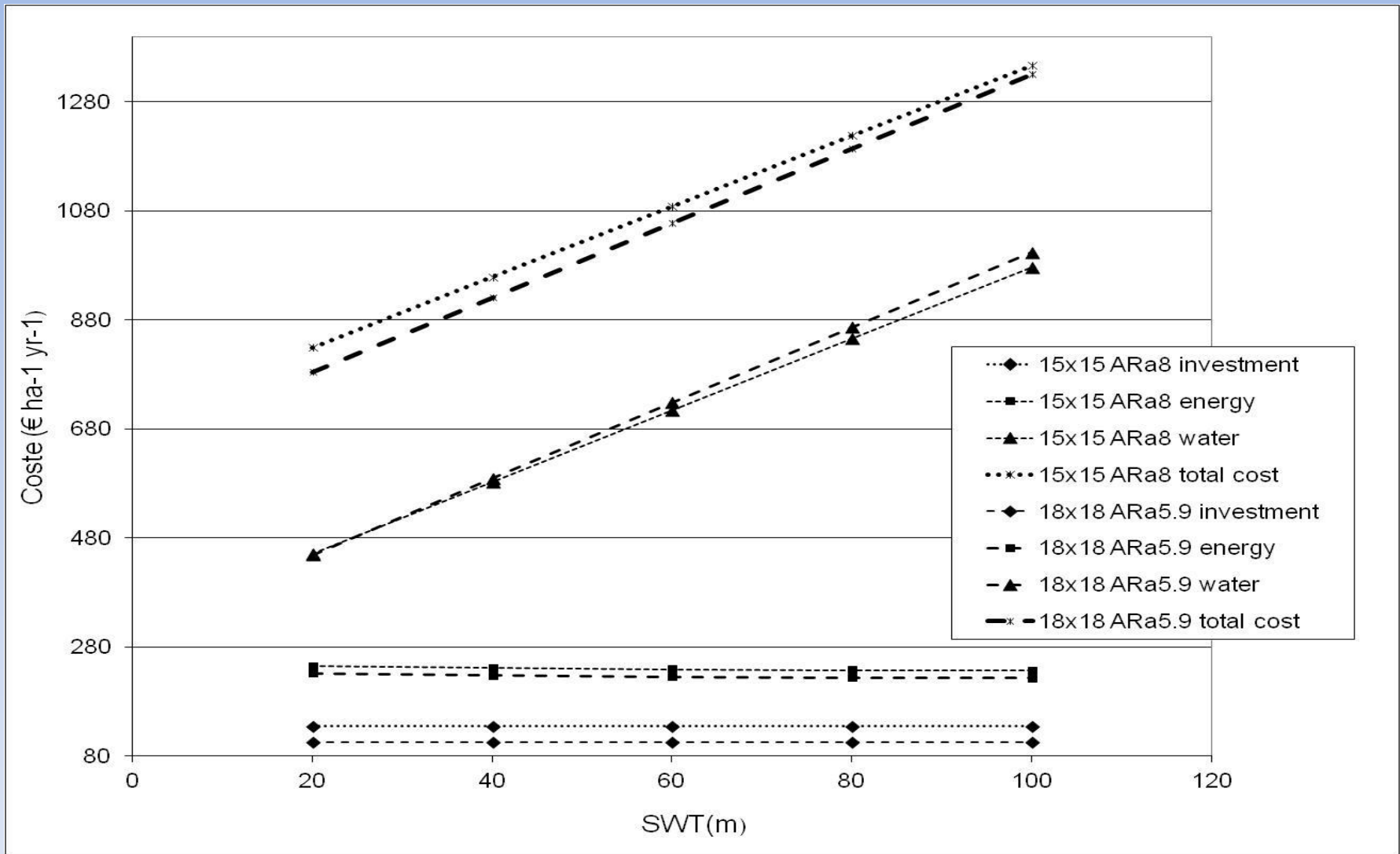


Lower C_T for 18x18 with $AR_a = 5.9 \text{ mm h}^{-1}$ and $NS = 12$

Pattern of C_T with the S for pipe and vineyard

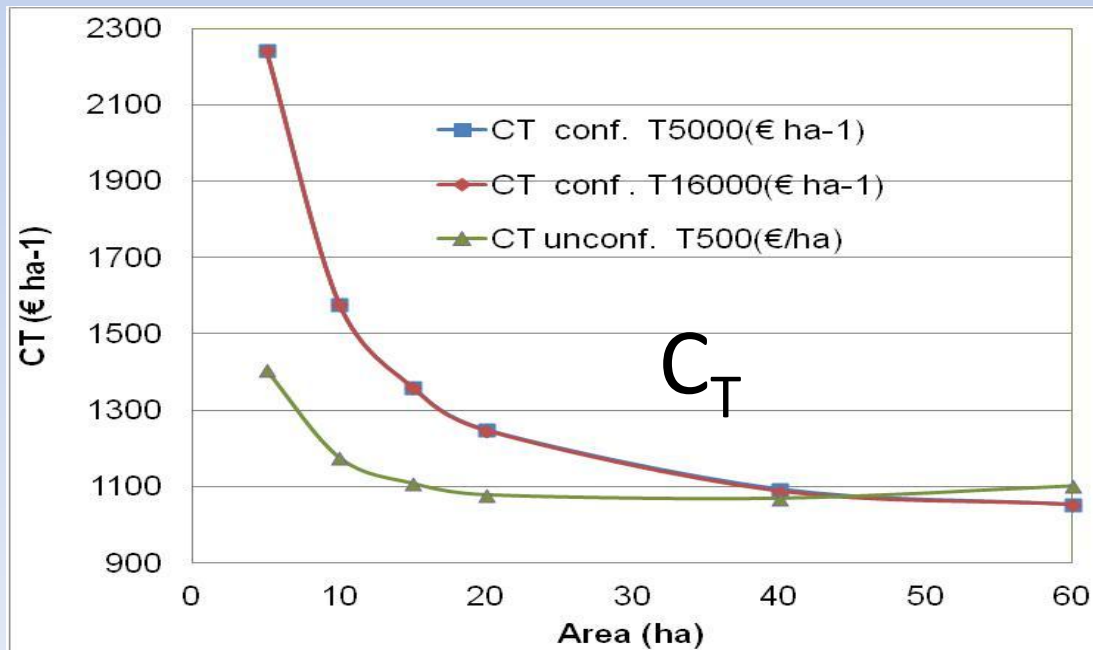
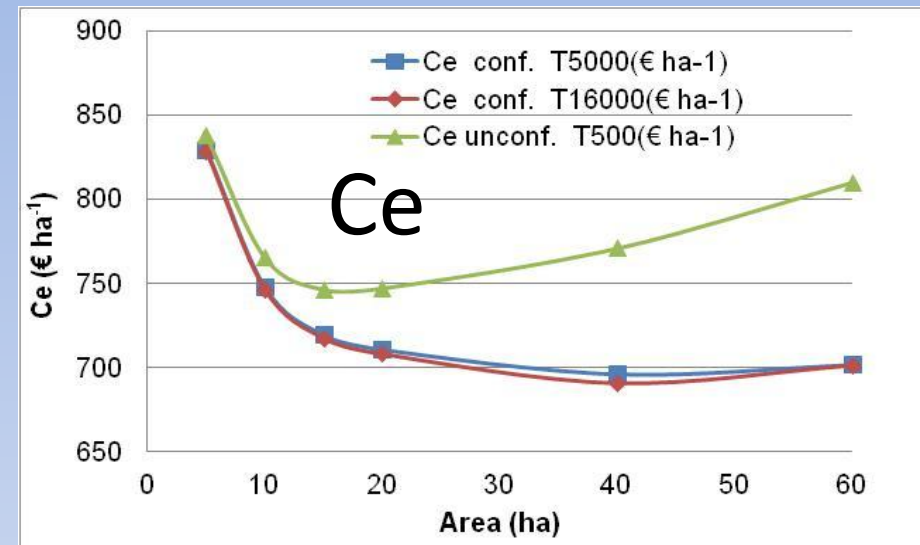
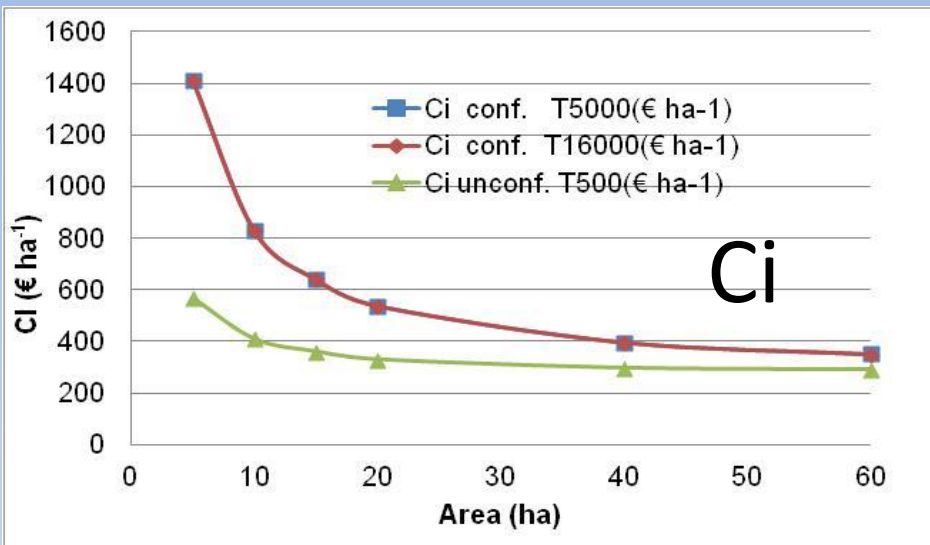


Components of C_T (C_w , $C_{as}+C_{ms}$, C_{es}), for different SWT for $S=20$ ha $NS=12$ for 18×18 (1.66 ha) and $NS=15$ for 15×15 (1.33 ha)



Sprinkler spacing, h_0 and ARA have low influence in C_T

Comparison between **unconfined** and **confined** aquifer for 18x18, $ARa=6.33 \text{ mm h}^{-1}$ and SWL= 60 m



CONCLUSIONES

- For the case studies **energy** represent **up to 70% of the cost** of water application in plot.
- It is very important the **proper pump selection** and its **operation time** (into the energy rate periods) throughout the irrigation season
- The water cost (C_w) is mainly conditioned by the transmissivity (**T values**), the proper **pump** selection and the **borehole and pumping pipes**, (directly interrelated).
- DC-WAT tool, adaptable to the specific conditions of investment and energy cost in each country, is useful for **analyze the irrigation system as a whole**, from the water source to the emitter, integrating the main factors implied in the process.